high partitions shall have a minimum of one manual control (on/off switch) for lighting in that space. Additional manual controls shall be provided for each task location or for each group of task locations within an area of 450 ft² or less. For spaces with only one lighting fixture or with a single ballast, one manual control is required. Exceptions are as follows:

401.3.4.2.1 Continuous lighting for security;

401.3.4.2.2 Systems in which occupancy sensors, local programmable timers, or three-level (including OFF) step controls or preset dimming controls are substituted for manual controls at the rate of one for every two required manual controls, providing at least one control is installed for every 1500 watts of power.

401.3.4.2.3 Systems in which four-level (including OFF) step controls or preset dimming controls or automatic or continuous dimming controls are substituted for manual controls at a rate of one for every three required manual controls, providing at least one control is installed for every 1500 watts of power.

401.3.4.2.4 Spaces that must be used as a whole, such as public lobbies, retail stores, warehouses, and storerooms.

401.3.4.3 Multiple Location Controls. Manual controls that operate the same load from multiple locations must be counted as one manual control.

401.3.4.4 Control Accessibility. Lighting controls shall be readily accessible from within the space controlled. Exceptions are as follows: Controls for spaces that are to be used as a whole, automatic controls, programmable controls, controls requiring trained operators, and controls for safety hazards and security.

401.3.4.5 Hotel and Motel Guest Room Control. Hotel and motel guest rooms and suites shall have at least one master switch at the main entry door that controls all permanently wired lighting fixtures and switched receptacles excluding bathrooms. The following exception applies: Where switches are provided at the entry to each room of a multiple-room suite.

401.3.4.6 Switching of Exterior Lighting. Exterior lighting not intended for

24-hour use shall be automatically switched by either timer or photocell or a combination of timer and photocell. When used, timers shall be capable of seven-day and seasonal daylight schedule adjustment and have power backup for at least four hours.

401.3.5 Ballasts.

401.3.5.1 Tandem Wiring. One-lamp or three-lamp fluorescent luminaries that are recess mounted within 10 ft center-to-center of each other, or pendant mounted, or surface mounted within 1 ft of each other, and within the same room, shall be tandem wired, unless three-lamp ballasts are used.

401.3.5.2 Power Factor. All ballasts shall have a power factor of at least 90%, with the exception of dimming ballasts, and ballasts for circline and compact fluorescent lamps and low wattage high intensity discharge (HID) lamps not over 100 W.

§ 434.402 Building envelope assemblies and materials.

The building envelope and its associated assemblies and materials shall meet the provisions of this section.

402.1 Calculations and Supporting Information.

402.1.1 Material Properties. Information on thermal properties, building envelope system performance, and component heat transfer shall be obtained from RS-4. When the information is not available from RS-4, (incorporated by reference, see §434.701) the data shall be obtained from manufacturer's information or laboratory or field test measurements using RS-5, RS-6, RS-7, or RS-8 (incorporated by reference, see §434.701).

402.1.1.1 The shading coefficient (SC) for fenestration shall be obtained from RS-4 (incorporated by reference, see $\S434.701$) or from manufacturer's test data. The shading coefficient of the fenestration, including both internal and external shading devices, is SC_x and excludes the effect of external shading projections, which are calculated separately. The shading coefficient used for louvered shade screens shall be determined using a profile angle of 30 degrees as found in Table 41, Chapter 27 of RS-4 (incorporated by reference, see $\S434.701$).

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402.1.2 Thermal Performance Calculations. The overall thermal transmittance of the building envelope shall be

calculated in accordance with Equation 402.1.2:

$$U_o = \sum U_i A_i / A_o = (U_1 A_1 + U_2 A_2 + \dots + U_n A_n) / A_o$$
 (402.1.2)

Where:

U_o = the area-weighted average thermal transmittance of the gross area of the building envelope; *i.e.*, the exterior wall assembly including fenestration and doors, the roof and ceiling assembly, and the floor assembly, Btu/(h·ft².ºF)

 A_o = the gross area of the building envelope,

 $\begin{array}{l} U_i = the \ thermal \ transmittance \ of \ each \ individual \ path \ of \ the \ building \ envelope, \ \emph{i.e.}, \\ the \ opaque \ portion \ or \ the \ fenestration, \\ Btu/(h\cdot ft^{2.\circ}F) \end{array}$

 $U_i = 1/R_i$ (where R_i is the total resistance to heat flow of an individual path through the building envelope)

 A_i = the area of each individual element of the building envelope, ft^2

The thermal transmittance of each component of the building envelope shall be determined with due consideration of all major series and parallel heat flow paths through the elements of the component and film coefficients and shall account for any compression of insulation. The thermal transmittance of opaque elements of assemblies shall be determined using a series path procedure with corrections for the presence of parallel paths within an element of the envelope assembly (such as wall cavities with parallel paths through insulation and studs). The thermal performance of adjacent ground in below-grade applications shall be excluded from all thermal calculations.

402.1.2.1 Envelope Assemblies Containing Metal Framing. The thermal transmittance of the envelope assembly containing metal framing shall be determined from one of three methods:

(a) Laboratory or field test measurements based on RS-5, RS-6, RS-7, or RS-8 (incorporated by reference, see § 434.701).

(b) The zone method described in Chapter 22 of RS-4 (incorporated by reference, see §434.701) and the formulas on page 22.10.

(c) For metal roof trusses or metal studs covered by Tables 402.1.2.1a and b, the total resistance of the series path shall be calculated in accordance with the following Equations:

$$U_i = 1/R_t$$

$$R_t = R_i + R_e$$
Equation 402.1.2.1a

Where:

 $R_{\tau} = the \ total \ resistance \ of \ the \ envelope \ assembly$

 R_i = the resistance of the series elements (for i = 1 to n) excluding the parallel path element(s)

 R_e = the equivalent resistance of the element containing the parallel path (R-value of insulation \times F_c). Values for F_c and equivalent resistances shall be taken from Tables 402.1.2.1a or b.

TABLE 402.1.2.1A—PARALLEL PATH CORRECTION FACTORS—METAL ROOF TRUSSES SPACED 4 FT. O.C. OR GREATER THAT PENETRATE THE INSULATION

Effective framing cavity R-values	Correction factor F _c	Equivalent resistance R _e 1
R-0	1.00	R-0
R-5	0.96	R-4.8
R-10	0.92	R-9.2
R-15	0.88	R-13.2
R-20	0.85	R-17.0
R-25	0.81	R-20.3
R-30	0.79	R-23.7
R-35	0.76	R-26.6
R-40	0.73	R-29.2
R-45	0.71	R-32.0
R-50	0.69	R-34.5
R-55	0.67	R-36.0

 $^{\rm 1}\textsc{Based}$ on 0.66-inch-diameter cross members every one foot.

TABLE 402.1.2.1B—PARALLEL PATH CORRECTION FACTORS—METAL FRAMED WALLS WITH STUDS 16 GA. OR LIGHTER

Size of members	Spacing of framing, in.	Cavity insulation R- Value	Correction factor F _c	Equivalent resistance R _e
2 × 4	16 O.C.	R-11 R-13	0.50 0.46	R–5.5 R–6.0
2×4	24 O.C.	R–15 R–11 R–13 R–15	0.43 0.60 0.55 0.52	R-6.4 R-6.6 R-7.2 R-7.8
2 × 6	16 O.C.	R-19 R-21	0.37 0.35	R-7.1 R-7.4
2×6	24 O.C.	R-19 R-21	0.45 0.43	R-8.6 R-9.0
2 × 8	16 O.C. 24 O.C.	R-25 R-25	0.31 0.38	R-7.8 R-9.6

402.1.2.2 Envelope Assemblies Containing Nonmetal Framing. The thermal transmittance of the envelope assembly shall be determined from laboratory or field test measurements based on RS-5, RS-6, RS-7, or RS-8 (incorporated by reference, see §434.701) or from the series-parallel (isothermal planes) method provided in page 23.2 of Chapter 23 of RS-4 (incorporated be reference, see §434.701).

402.1.2.3 Metal Buildings. For elements with internal metallic structures bonded on one or both sides to a metal skin or covering, the calculation

procedure specified in RS-9 (incorporated by reference, see §434.701) shall be used.

402.1.2.4 Fenestration Assemblies. Determine the overall thermal transmittance of fenestration assemblies in accordance with RS-18 and RS-19 (incorporated by reference, see § 434.701) or by calculation. Calculation of the overall thermal transmittance of fenestration assemblies shall consider the center-ofglass, edge-of-glass, and frame components.

(a) The following equation 402.1.2.4a shall be used.

$$\begin{split} U_{of} = & \left[\sum_{i=1}^{n} \left(U_{cg,i} \times A_{cg,i} + U_{eg,i} \times A_{eg,i} + U_{f,i} \times A_{f,i} \right) \right] / \left[\sum_{i=1}^{n} \left(A_{cg,i} + A_{eg,i} + A_{f,i} \right) \right] \\ = & \left(U_{cg,l} \times A_{cg,l} + U_{eg,l} \times A_{eg,l} + U_{f,l} \times A_{f,l} + U_{cg,2} \times A_{cg,2} + U_{eg,2} \times A_{eg,2} + U_{f,2} \times A_{f,2} + \dots U_{cg,n} \times A_{cg,n} \right. \\ & \left. + U_{eg,n} \times A_{eg,n} + U_{f,n} \times A_{f,n} \right) / \left(A_{cg,l} + A_{eg,l} + A_{f,l} + A_{cg,2} + A_{eg,2} + A_{f,2} + \dots A_{cg,n} + A_{eg,n} + A_{f,n} \right) \\ & \left. U_{of} = \left[\sum_{i=1}^{n} \left(U_{cg,i} \times A_{cg,i} + U_{eg,i} \times A_{eg,i} + U_{f,i} \times A_{f,i} \right) \right] / \left[\sum_{i=1}^{n} \left(A_{cg,i} + A_{eg,i} + A_{f,i} \right) \right] \\ & = \left(U_{cg,l} \times A_{cg,l} + U_{eg,l} \times A_{eg,l} + U_{f,l} \times A_{f,l} + U_{cg,2} \times A_{cg,2} + U_{eg,2} \times A_{eg,2} + U_{f,2} \times A_{f,2} \right. \\ & \left. + \dots U_{cg,n} \times A_{cg,n} + U_{eg,n} \times A_{cg,n} + U_{f,n} \times A_{f,n} \right) / \left(A_{cg,l} + A_{eg,l} + A_{f,l} + A_{cg,2} + A_{eg,2} + A_{f,2} \right. \\ & \left. + \dots A_{cg,n} + A_{eg,n} + A_{f,n} \right) \end{aligned}$$

Where:

 $\begin{array}{lll} U_{of} = the \ overall \ thermal \ transmittance \ of \\ the \ fenestration \ assemblies, \ including \ the \\ center-of-glass, \ edge-of-glass, \ and \ frame \\ components, \ Btu/(h\cdot ft^2\cdot {}^\circ F) \end{array}$

 $i = numerical \ subscript \ (1,\ 2,\ \dots n) \ refers \ to \\ each \ of \ the \ various \ fenestration \ types \\ present in \ the \ wall$

n = the number of fenestration assemblies in the wall assembly $U_{\rm cg}$ = the thermal transmittance of the center-of-glass area, $Btu/(h\cdot ft^2\cdot {}^\circ F)$

 A_{cg} = the center of glass area, that is the overall visible glass area minus the edge-of-glass area, ft^2

 $\begin{array}{l} U_{\rm eg} = the \ thermal \ transmittance \ of \ the \ edge \\ of \ the \ visible \ glass \ area \ including \ the \ effects \ of \ spacers \ in \ multiple \ glazed \ units, \\ Btu/(h\cdot ft^2\cdot {}^\circ F) \end{array}$

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 A_{eg} = the edge of the visible glass area, that is the 2.5 in. perimeter band adjacent to the frame ft²

 U_f = the thermal transmittance of the frame area. Btu/(h·ft²·°F)

 $A_{\rm f}$ = the frame area that is the overall area of the entire glazing product minus the center-of-glass area and minus the edge-of-glass area, ${\rm ft^2}$

(b) Values of $U_{\rm of}$ shall be based on one of the following methods:

(1) Results from laboratory test of center-of-glass, edge-of-glass, and frame assemblies tested as a unit at winter conditions. One of the procedures in Section 8.3.2 of RS-1 (incorporated by reference, see § 434.701) shall be used.

(2) Overall generic product C (commercial) in Table 13, Chapter 27, of the RS-4 (incorporated by reference, see §434.701). The generic product C in Table 13, Chapter 27, is based on a product of 24 ft². Larger units will produce lower U-values and thus it is recommended to use the calculation procedure detailed in Equation 402.1.2.4a.

(3) Calculations based on the actual area for center-of-glass, edge-of-glass, and frame assemblies and on the thermal transmittance of components derived from 402.1.2.4a, 402.1.2.4b or a combination of the two.

402.1.3 Gross Areas of Envelope Components.

402.1.3.1 Roof Assembly. The gross area of a roof assembly shall consist of the total surface of the roof assembly exposed to outside air or unconditioned spaces and is measured from the exterior faces of exterior walls and centerline of walls separating buildings. The roof assembly includes all roof or ceiling components through which heat may flow between indoor and outdoor environments, including skylight surfaces but excluding service openings. For thermal transmittance purposes when return air ceiling plenums are employed, the roof or ceiling assembly

shall not include the resistance of the ceiling or the plenum space as part of the total resistance of the assembly.

402.1.3.2 Floor Assembly. The gross area of a floor assembly over outside or unconditioned spaces shall consist of the total surface of the floor assembly exposed to outside air or unconditioned space and is measured from the exterior face of exterior walls and centerior of walls separating buildings. The floor assembly shall include all floor components through which heat may flow between indoor and outdoor or unconditioned space environments.

402.1.3.3 Wall Assembly. The gross area of exterior walls enclosing a heated or cooled space is measured on the exterior and consists of the opaque walls, including between-floor spandrels, peripheral edges of flooring, window areas (including sash), and door areas but excluding vents, grilles, and pipes.

402.2 Air Leakage and Moisture Mitigation. The requirements of this section shall apply only to those building components that separate interior building conditioned space from the outdoors or from unconditioned space or crawl spaces. Compliance with the criteria for air leakage through building components shall be determined by tests conducted in accordance with RS-10 (incorporated by reference, see § 434.701).

402.2.1 *Air Barrier System.* A barrier against leakage shall be installed to prevent the leakage of air through the building envelope according to the following requirements:

(a) The air barrier shall be continuous at all plumbing and heating penetrations of the building opaque wall.

(b) The air barrier shall be sealed at all penetrations of the opaque building wall for electrical and telecommunications equipment.

TABLE 402.2.1—AIR LEAKAGE FOR FENESTRATION AND DOORS MAXIMUM ALLOWABLE INFILTRATION RATE

Component	Reference standard	cfm/lin ft Sash crack or cfm/ft² of area
Fenestration Aluminum:		
Operable	RS-11*	0.37 cfm/lin ft.
Jalousie	RS-11*	1.50 cfm/ft ² .
Fixed	RS-11*	0.15 cfm/ft ² .

TABLE 402.2.1—AIR LEAKAGE FOR FENESTRATION AND DOORS MAXIMUM ALLOWABLE INFILTRATION RATE—Continued

Component	Reference standard	cfm/lin ft Sash crack or cfm/ft² of area
Poly Vinyl Chloride (PVC):		
Prime Windows	RS-12*	0.37 cfm/ft ² .
Wood:		
Residential	RS-13*	0.37 cfm/ft ² .
Light Commercial	RS-13*	0.25 cfm/ft ² .
Heavy Commercial	RS-13*	0.15 cfm/ft ² .
Sliding Glass Doors:		
Aluminum	RS-11*	0.37 cfm/ft ² .
PVC	RS-12*	0.37 cfm/lin ft.
Doors—Wood:		
Residential	RS-14*	0.34 cfm/ft ² .
Light Commercial	RS-14*	0.25 cfm/ft ² .
Heavy Commercial	RS-14*	0.10 cfm/ft ² .
Commercial Entrance Doors	RS-10*	1.25 cfm/ft ² .
Residential Swinging Doors	RS-10*	0.50 cfm/ft ² .
Wall Sections Aluminum	RS-10*	0.06 cfm/ft ² .

NOTE: [The "Maximum Allowable Infiltration Rates" are from current standards to allow the use of available products.] *Incorporated by reference, see § 434.701.

- 402.2.2 Building Envelope. The following areas of the building envelope shall be sealed, caulked, gasketed, or weatherstripped to limit air leakage:
- (a) Intersections of the fenestration and door frames with the opaque wall sections.
- (b) Openings between walls and foundations, between walls and roof and wall panels.
- (c) Openings at penetrations of utility service through, roofs, walls, and floors.
 - (d) Site built fenestration and doors.
- (e) All other openings in the building envelope.

Exceptions are as follows: Outside air intakes, exhaust outlets, relief outlets, stair shaft, elevator shaft smoke relief openings, and other similar elements shall comply with subsection 403.

402.2.2.1 Fenestration and Doors Fenestration and doors shall meet the requirements of Table 402.2.1.

402.2.2.2 Building Assemblies Used as Ducts or Plenums. Building assemblies used as ducts or plenums shall be sealed, caulked, and gasketed to limit air leakage.

402.2.2.3 Vestibules. A door that separates conditioned space from the exterior shall be equipped with an enclosed vestibule with all doors opening into and out of the vestibule equipped with self-closing devices. Vestibules shall be designed so that in passing through the vestibule, it is not necessary for the in-

terior and exterior doors to open at the same time. Exceptions are as follows: Exterior doors need not be protected with a vestibule where:

- (a) The door is a revolving door.
- (b) The door is used primarily to facilitate vehicular movement or material handling.
- (c) The door is not intended to be used as a general entrance door.
- (d) The door opens directly from a dwelling unit.
- (e) The door opens directly from a retail space less than 2,000 ft² in area, or from a space less than 1,500 ft² for other uses.
- (f) In buildings less than three stories in building height in regions that have less than 6,300 heating degree days base 65°F.
- 402.2.2.4 Compliance Testing. All buildings shall be tested after completion using the methodology in RS-11, (incorporated by reference, see § 434.701) or an equivalent approved method to determine the envelope air leakage. A standard blower door test is an acceptable technique to pressurize the building if the building is 5,000 ft² or less in area. The buildings's air handling system can be used to pressurize the building if the building is larger than 5,000 ft². The following test conditions shall be:
- (a) The measured envelope air leakage shall not exceed 1.57 pounds per

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square foot of wall area at a pressure difference of 0.3 inches water.

- (b) At the time of testing, all windows and outside doors shall be installed and closed, all interior doors shall be open, and all air handlers and dampers shall be operable. The building shall be unoccupied.
- (c) During the testing period, the average wind speed during the test shall be less than 6.6 feet per second, the average outside temperature greater than 59°F, and the average inside-outside temperature difference is less than 41°F.
- 402.2.2.5 Moisture Migration. The building envelope shall be designed to limit moisture migration that leads to deterioration in insulation or equipment performance as determined by the following construction practices:
- (a) A vapor retarder shall be installed to retard, or slow down the rate of water vapor diffusion through the building envelope. The position of the vapor retarder shall be determined taking into account local climate and indoor humidity levels. The methodologies presented in Chapter 20 of RS-4 (incorporated by reference, see § 434.701) shall be used to determine temperature and water vapor profiles through the envelope systems to assess the potential for condensation within the envelope and to determine the position of the vapor retarder within the envelope system.
- (b) The vapor retarder shall be installed over the entire building envelope.
- (c) The perm rating requirements of the vapor retarder shall be determined using the methodologies contained in Chapter 20 of RS-4, (incorporated by reference, see §434.701) and shall take into account local climate and indoor humidity level. The vapor retarder shall have a performance rating of 1 perm or less.

402.3 Thermal Performance Criteria.

402.3.1 Roofs; Floors and Walls Adjacent to Unconditioned Spaces. The area weighted average thermal transmittance of roofs and also of floors and walls adjacent to unconditioned spaces shall not exceed the criteria in Table 402.3.1a. Exceptions are as follows: Skylights for which daylight credit is taken may be excluded from the cal-

culations of the roof assembly $U_{\rm or}$ if all of the following conditions are met:

- (a) The opaque roof thermal transmittance is less than the criteria in Table 402.3.1b.
- (b) Skylight areas, including framing, as a percentage of the roof area do not exceed the values specified in Table 402.3.1b. The maximum skylight area from Table 402.3.1b may be increased by 50% if a shading device is used that blocks over 50% of the solar gain during the peak cooling design condition. For shell buildings, the permitted skylight area shall be based on a light level of 30 foot candles and a lighting power density (LPD) of less than 1.0 w/ ft2. For speculative buildings, the permitted skylight area shall be based on the unit lighting power allowance from Table 401.3.2a and an illuminance level as follows: for LPD < 1.0, use 30 footcandles; for 1.0 < LPD < 2.5, use 50 footcandles; and for LPD ≥ 2.5 , use 70 footcandles.
- (c) All electric lighting fixtures within daylighted zones under skylights are controlled by automatic daylighting controls.
- (d) The U_o of the skylight assembly including framing does not exceed Btu/(h·ft $^{2.\circ}F)$ [Use 0.70 for ≤ 8000 HDD65 and 0.45 for >8000 HDD65 or both if the jurisdiction includes cities that are both below and above 8000 HDD65.]
- (e) Skylight curb U-value does not exceed 0.21 Btu/ $(h \cdot ft^{2 \cdot \circ}F)$.
- (f) The infiltration coefficient of the skylights does not exceed 0.05 cfm/ft².
- 402.3.2 Below-Grade Walls and Slabson-Grade. The thermal resistance (R-value) of insulation for slabs-on-grade, or the overall thermal resistance of walls in contact with the earth, shall be equal to or greater than the values in Table 402.3.2.
- 402.4 Exterior Walls. Exterior walls shall comply with either 402.4.1 or 402.4.2.

402.4.1 Prescriptive Criteria. (a) The exterior wall shall be designed in accordance with subsections 402.4.1.1 and 402.4.1.2. When the internal load density range is not known, the 0-1.50 W/ft² range shall be used for residential, hotel/motel guest rooms, or warehouse occupancies; the 3.01-3.50 w/ft² range shall be used for retail stores smaller

(b) When more than one condition exists, area weighted averages shall be used. This requirement shall apply to all thermal transmittances, shading coefficients, projection factors, and internal load densities rounded to the same number of decimal places as shown in the respective table.

402.4.1.1 Opaque Walls. The weighted average thermal transmittance (U-value) of opaque wall elements shall be less than the values in Table 402.4.1.1. For mass walls (HC \geq 5), criteria are presented for low and high window/wall ratios and the criteria shall be determined by interpolating between these values for the window/wall ratio of the building.

402.4.1.2 Fenestration. The design of the fenestration shall meet the criteria of Table 402.4.1.2. When the fenestration columns labeled "Perimeter Daylighting" are used, automatic daylighting controls shall be installed in the perimeter daylighted zones of the building. These daylighting controls shall be capable of reducing electric lighting power to at least 50% of full power. Only those shading or lighting controls for perimeter daylighting that are shown on the plans shall be considered. The column labeled "VLT > = SC" shall be used only when the shading coefficient of the glass is less than its visible light transmittance.

APPENDIX A

The example Alternate Component Package tables illustrate the requirements of subsections 434.301.1, 434.402.3.1, 434.402.3.2, 434.402.4.1.1 and 434.402.4.1.2. Copies of specific tables contained in this Appendix A can be obtained from the Energy Code for Federal Commercial Buildings, Docket No. EE-RM-79-112-C, EE-43, Office of Building Research and Standards, U.S. Department of Energy, Room 1J-018, 1000 Independence Avenue, SW., Washington, DC 20585, (202) 586-9127.

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ABLE 40	02.4.1.2 MA	TABLE 402.4.1.2 MAXIMUM WINDOW WALL RATIO (WWR)	OW WAL	L RATIO (WWR)		
			Fene	Fenestration U-Factor (Uof)	actor (U	fe	
Internal	Projection Factor	Shading Coefficient	Base	Case	Perime	ter Day	Perimeter Daylighting
Density	(PF)	(SCx)	1.23 0	0.72	1.23	0.72	0.72
(ILD) Range	Range	Range	to 0.73	to N/A	o to	o 0	o 0
24		1.00 - 0.72	L	13	17	17	18
	-		19	18	22	21	22
	0.00	0.60 - 0.51	23	22	27	56	27
	0.25		53	. 28	34	32	34
		0.38 - 0.26	2 S	39	S 8	\$ 2	* 4 * 7
			30	21	36	25	36
00.0	0.26 -	0.71 - 0.61	ន	27	£	32	3 8
1.50	0.50	0.60 - 0.51	36	34	43	9	4
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-		1.00 - 0.72	12	12	70	61	21
		0.71 - 0.61	16	15	56	22	27
	0.00	0.60 - 0.51	61	19	32	3	33
	0.25	0.50 - 0.39	54	73	4	% ;	41
		0.38 - 0.26	34	32	3 8	7 8	2 8
			8 2	18	7	2	33
1.51	0.26 -	0.71 - 0.61	24	23	4	3 6	4 8
3.00	0.50	0.60 - 0.51	59	28	22	46	49
		0.50 - 0.39	37	35	89	\$3	62
		0.38 - 0.00	22	20	66	83	68
		1.00 - 0.72	2 2	24	4	4 :	4 2
	+ 00.0	0.71-0.01	3 5	30	3 5	3 5	8 6
		0.50 - 0.00	2 92	. 8	8	\$ 6	2 &
		1.00 - 0.72	6	6	18	17	50
	:	0.71 - 0.61	12	12	23	22 :	56
	0.00	0.60 - 0.51	2 2	<u> </u>	3 5	7.	- F
	C7:0	0.30 - 0.39	9 %	74	3 5	£ 8	3,8
		0.25 - 0.00	. *	43	8	£	8 8
		1.00 - 0.72	14	13	78	56	30
3.01	0.26	0.71 - 0.61	8:	11	37	£ :	38
3.50	0.50	0.60 - 0.51	2 2	7 7	\$:	4 :	4 9
		0.38 - 0.00	\$ 5	9.89	2 2	; F	8 8
		1.00 - 0.72	61	18	4	37	14
	0.50 +	0.71 - 0.61	25	24	\$\$	49	24
		0.60 - 0.51	33	29	2 2	3 2	19
		0.50 - 0.00	7	3,	1	٩	50

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TABLE 301.1 EXTERIOR DESIGN CONDITIONS WINTER Design Dry Bulb: 44°F; SISLAMER Design Dry Bulb: 90°F; Mean Coincident Wer Bulb Annual Operating Hours, 8AM. 4PM when 55°Fc~TC~60°F;	EXTERIO gn Dry Bulb ign Dry Bul ing Hours, 8	R DESIGN Co 1: 44°F; b: 90°F; Meau AM - 4PM w	iN CONDITIONS Mean Coincident Wet Bulb: M when 55ºFc=T<=69ºF: 7	Wet Bulb: <=69ºF; ∑	HDD65: :77°F; CDD65: 259	65: 185 55: 4045
TABLE 4023.1(A) MAX. THERMAL TRANSMITTANCE (U) Roof Wall adjacent to unconditioned space	LE 402.3.1(A) MAX. THERMA adjacent to unconditioned space	THERMAL ned space	TKANSMI	TANCE (U	0.075	
Floor over unconditioned space	onditioned sp	ace			0.400	
TABLE 402.3.1(B) MAX. EXEMPT SKYLIGHT AREA	1(B) MAX.	EXEMPT SK	YLIGHT A	REA AS %	% OF ROOF AREA	REA
Transmittance (VLT)	× (VLT)	Ft. Candles	<1.00	1.00 - 1.50	1.00 - 1.50 1.51 - 2.00 >	>2.00
92.0		8 S S	3.1	3.1 4.3	3.9 5.5	L.
0.50		2 8 8 8	24 8.4 8.4 8.4 8.9	S 4 8 8 4 8	6.0 8.4 10.2	7.2 10.2 12.0
TABLE 402.3.2 MINIMUM THERMAL RESISTANCE (R. VALUE)	2 MINIMU	M THERMA	L RESISTA	NCE (R-VA	LUE)	
Slab on grade:	Unheated / Heated:	Heated:		24 inches	36 inches	48 inches
•	Horizontal			R-0/R-2	R-0/R-2	R-0/R-2
Wall below grade:	Vertical ide:			K-0/K-2	R-0/R-2	K-0/K-2
2011	3771	Contraction of the state of the	100	101010101	1	
1ADLE 402.4.	I.I MAA.	WALL THEK	MAL IKA	Inch	INCE (Uow)	uoi
ILD Range	WWR	HC Range	ange	Interior/Integral		Exterior
All	0 to 100	0.0	- 4.9	1.000		1.000
			6.6-	1.000		1.000
0.00 to 1.50	2	15.0	- 14.9	1.000		000
			- 9.9	1.000		1.000
	86	10.0	- 14.9	1.000		000
		5.0	-9.9	1.000		1.000
	12	10.0	- 14.9	1.000		1.000
1.51 to 3.00			00	1,000		000
	8		-149	1.000		1.000
			+	1.000		1.000
	۰	0.8	-9.9	1.000		1.000
3.01 to 3.50	^		- 14.7	1.000		1.000
			- 6.6	1.000		1.000
	83	10.0	- 14.9	1.000		000
		0.01		1.000		1.000

402.4.2 System Performance Criteria. The cumulative annual energy flux attributable to thermal transmittance and solar gains shall be less than the criteria determined using the ENVSTD24 computer program in Standard 90.1–1989, or the equations in

RS-1, (incorporated by reference, see §434.701) Attachment 8-B. The cumulative annual energy flux shall be calculated using the ENVSTD24 computer program or the equations in RS-1, (incorporated by reference, see §434.701) Attachment 8-B.

TABLE 402.4.2—EQUIP DEFAULT VALUES FOR ENVSTD24

Occupancy	Default equip- ment power density ¹	Default occu- pant load ad- justment ¹	Default ad- justed equip- ment power density
Assembly	0.25	0.75	1.00
Health/Institutional	1.00	-0.26	0.74
Hotel/Motel	0.25	-0.33	0.00
Warehouse/Storage	0.10	-0.60	0.00
Multi-Family High Rise	0.75	N/A	0.00
Office	0.75	- 0.35	0.40
Restaurant	0.10	0.07	0.17
Retail	0.25	-0.38	0.00
School	0.50	0.30	0.80

¹ Defaults as defined in Section 8.6.10.5, Table 8–4, and Sections 8.6.10.6 and 13.7.2.1, Table 13–2 from RS–1 (incorporated by reference, see §434.701).

402.4.2.1 Equipment Power Density (EQUIP). The equipment power density used in the ENVSTD24 computer program shall use the actual equipment power density from the building plans and specifications or be taken from Table 402.4.2 using the column titled "Default Adjusted Equipment Power Density" or calculated for the building using the procedures of RS-1. (incorporated by reference, see §434.701). The program limits consideration of the equipment power density to a maximum of $1\,\mathrm{W/ft^2}$.

402.4.2.2 Lighting Power Density (LIGHTS). The lighting power density used in the ENVSTD24 computer program shall use the actual lighting power density from the building plans and specifications or the appropriate value from Tables 401.3.2a, b, c, or d.

402.4.2.3 Daylighting Control Credit Fraction (DLCF). When the daylighting control credit fraction is other than zero, automatic daylighting controls shall be installed in the appropriate perimeter zones(s) of the building to justify the credit.

§ 434.403 Building mechanical systems and equipment.

Mechanical systems and equipment used to provide heating, ventilating, and air conditioning functions as well as additional functions not related to space conditioning, such as, but not limited to, freeze protection in fire projection systems and water heating, shall meet the requirements of this section.

403.1 Mechanical Equipment Efficiency. When equipment shown in Tables 403.1a through 403.1f is used, it shall have a minimum performance at the specified rating conditions when tested in accordance with the specified reference standard. The reference standards listed in Tables 403.1a through 403.1f are incorporated by reference, see §434.701. Omission of minimum performance requirements for equipment not listed in Tables 403.1a through 403.1f does not preclude use of such equipment.

TABLE 403.1A—UNITARY AIR CONDITIONERS AND CONDENSING UNITS, ELECTRICALLY OPERATED, MINIMUM EFFICIENCY REQUIREMENTS

Equipment type	Size category	Subcategory or rating condition	Minimum Efficiency ²	Test procedure ¹
Air Conditioners, Air Cooled.	< 65,000 Btu/h	Split system	10.0 SEER	ARI 210/240 (RS-15)* ARI 210/240 (RS-15)*
	≥ 240,000 Btu/h and < 760,000 Btu/h. ≥ 760,000 Btu/h	Split System and Single Package. Split System and Package	8.5 EER ³ 7.5 IPLV ³ 8.3 EER ³ 7.5 IPLV ³	ARI-340/360 (RS-16)* ARI-340/360 (RS-16)*